

## Piezoelectric Devices

The present invention relates to devices which use piezoelectric materials in their structure.

It is well known that piezoelectric material will contract and elongate when an alternating electric field is applied. On the other hand, if such a material is subjected to alternated strains an electric field will be induced. This effect is used in a number of known devices.

There is a desire to extend the use of piezoelectric materials to the fabrication of other devices and the present invention has been made against this background.

According to the present invention there is provided a device comprising a layer of piezoelectric material and a layer of ferroelectric material clamped together such that a voltage applied to one layer results in a voltage being generated across the other layer.

If two pieces of piezoelectric material are clamped together and a voltage applied to one of them, an induced voltage can be measured from the other. The ratio of the applied voltage will depend upon the piezoelectric properties of the two materials and, possibly, sample geometry. A piezoelectric amplifier/transformer can be realised in this way using two layers of piezoelectric material. In ceramic piezoelectric materials the strain and corresponding electric field are in-phase.

Ferroelectric materials are a sub-set of piezoelectric materials. They can exhibit a non-volatile, bi-stable internal polarisation (generally, with respect to a particular crystal axis). The state of polarisation is established by the application of a voltage between opposing surfaces of the material. Having applied a sufficiently large voltage to internally polarise the material, it is subsequently possible to determine the direction of polarisation. This operation consists of applying a voltage to set the polarisation in a specified direction. If the polarisation is already

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in that direction no charge exchange is required. However, if the polarisation is in the opposite direction a relatively large amount of charge exchange is required to establish the specified direction of polarisation. Thus, the previous direction of polarisation can be judged according to the high or low (zero) level of charge exchange required to establish the specified polarisation.

In the present invention it has been found that a polarised ferroelectric material elongates or contracts when a weak external field (much less than the coercive force of the ferroelectric material) is applied in parallel or anti-parallel, respectively, to the polarisation. Consequently, the strains induced along the polarisation axis can be in-phase or out-of-phase to the applied AC external field, depending on the direction of polarisation. Either strain or electric field can be the primary driving force in the piezoelectric effect and they have a linear relationship to the first order. From this it has been recognised, in the present invention, that the phase of the induced electric field of a polarised ferroelectric material can be controlled by the direction of polarisation.

The concepts of the present invention have been found to be beneficial for the implementation of a range of devices including analogue devices such as amplifiers/transducers, inverters and comparators.

Embodiments of the present invention will now be described in more detail, by way of further example only and with reference to the accompanying drawings, in which:-

Figure 1 illustrates the structure of an amplifier/transducer according to a first embodiment of the present invention; and

Figure 2 illustrates the structure of a comparator according to another embodiment of the present invention.

A first embodiment of the present invention is the implementation of an amplifier/transducer, the structure of which is illustrated in figure 1.

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A layer of polarised ferroelectric material can be used as a driving unit and apply an electric field to it as the input signal. The induced strain is then passed onto another layer of polarised ferroelectric material, the sensing unit. It induces a secondary electric field to provide the output signal. The magnification of the output depends on the properties of the materials used, while the phase of the signal is controlled by the arrangement of directions of polarisation in the two materials. Such a device acts as an amplifier or transformer with an extra degree of control on the phase of the output signal.

One structure to realise such an amplifier/transformer is to clamp these two units together along the polarisation axis, as shown in figure 1. The order of the units is not important.

Here the  $\epsilon_i$ ,  $d_{33,i}$ , and  $d_i$  are dielectric constant, piezoelectric coefficient and thickness of the material  $i$ , respectively. The strain of the material  $i$ ,  $S_{3,i}$  is simply:  $S_{3,i} = d_{33,i} E_{3,i}$  where  $E_{3,i}$  is the corresponding electric field component, and the stress is  $T_{3,i} = S_{3,i} / S_{33,i}$ . The subscript 3 indicates that the parameter concerned is the component along axis 3, the polarisation axis.

The performance of the device of figure 1 can be evaluated at two limits under hard-wall clamping conditions: (1) compressible limit; where the ferroelectric materials are regarded as compressible, which leads to  $(d_1 + d_2 = \text{constant})$  at all times; (2) incompressible limit; when the ferroelectric materials are regarded as incompressible, which gives  $T_{3,1} + T_{3,2} = 0$  where  $T_{3,i}$  is the stress in the material  $i$ . A real device should be working between these two limits.

At the compressible limit, we have  $\Delta(d_1 + d_2) = \Delta d_1 + \Delta d_2 = 0$ , and the induced change of the thickness at a given electric field is:

$$\begin{aligned} \Delta d_i(E_i) &= d_i(E_i) - d_i(0) \\ &\approx S_{3,i} d_i(0) \\ &= \pm d_{33,i} E_i d_i(0) \\ &\approx \pm d_{33,i} V_i \end{aligned}$$

where the sign +/- is chosen when the  $E_i$  is parallel/anti-parallel to the direction of polarisation. Therefore, the output signal is:

$$V_2 = \mp \frac{d_{33,1}}{d_{33,2}} V_1 \quad (1)$$

where the sign +/- shows that the input and output signals are in-phase/out-phase corresponding to anti-parallel/parallel polarisation between regions 1 and 2. The gain of the amplifier/transformer is  $d_{33,1} / d_{33,2}$ .

At the incompressible limit, we have  $T_{3,1} + T_{3,2} = 0$  and  $T_{3,i} = -e_{33,i} E_{3,i} \approx -e_{33,i} V_i / d_i(0)$  where  $e_{33,i}$  is another piezoelectric constant.

The output voltage shall be:

$$V_2 = \mp \frac{e_{33,1}}{e_{33,2}} \frac{d_{2(0)}}{d_{1(0)}} V_1 \quad (2)$$

where again the signs correspond to parallel and anti-parallel polarisation between regions 1 and 2, respectively, and the gain of the device in this case is  $e_{33,1} d_2(0) / e_{33,2} d_1(0)$ .

To compare with the analysis of the previously suggested piezoelectric amplifier/transformer, (other than at the above two limits) it becomes apparent that

$$T_{3,i} = c_{33,i} S_{3,i} = \pm c_{33,i} d_{33,i} E_{3,i}$$

where  $c_{33,i}$  is the elastic stiffness constant of the material  $i$ .

Since  $E_{3,i} \approx V_i / d_i(0)$ , the output can be expressed as:

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$$V_2 = \mp \frac{c_{33,1}}{c_{33,2}} \frac{d_{33,1}}{d_{33,2}} \frac{d_2(0)}{d_1(0)} V_1 \quad (3)$$

To the approximation of only one component involved, we have  $e_{33,i} = d_{33,i} c_{33,i}$  and find that Equation 3 is identical to Equation 2 obtained from the incompressible limit. From the same approximation, we can also have  $c_{33,i} = 1/s_{33,i}$  is the elastic compliance coefficient, and get:

$$V_2 = \mp \frac{d_{33,1}}{d_{33,2}} \frac{s_{33,2}}{s_{33,1}} \frac{d_2(0)}{d_1(0)} V_1 \quad (4)$$

Variation of the first embodiment leads to the implementation of an inverter. That is, when the properties and geometry of the materials concerned are chosen in such a way that the gain of the amplifier is unity, the device works as a inverter in the configuration of parallel polarisation.

Another embodiment of the present invention is the implementation of a comparator. If two identical driving units and one sensing unit are clamped together in the same way, it is possible to build up a comparator as shown in figure 2. The order of the units is again not important, if the input signals and output signal do not refer to one another. Otherwise, the arrangement as shown in figure 2 should be used. Besides, non-identical driving units can be used for special situations.

The performance of the comparator can be analysed in the same way as stated above in relation to the first embodiment. At the two limits, we now have: (1)  $\Sigma d_i = \text{constant}$ ; (2)  $(T_{3,11} + T_{3,12}) + T_{3,2} = 0$  if we assume that there is no interference between the two driving units. This assumption does affect the following conclusions drawn for the comparator.

In the first case, because  $\Sigma \Delta d_i = 0$ , we have:

$$\pm V_2 = - \frac{d_{33,1}}{d_{33,2}} (\pm V_{11} + \pm V_{12}) \quad (5)$$

where the signs refer to the applied field is parallel or anti-parallel to the corresponding polarisation.

Similarly, for the second case, we have

$$\pm V_2 = - \frac{d_{33,1}}{d_{33,2}} \frac{s_{33,2}}{s_{33,1}} \frac{d_{2(0)}}{d_{1(0)}} (\pm V_{11} + \pm V_{12}) \quad (6)$$

By arranging the directions of polarisation in the driving units as anti-parallel/parallel, we see the output of the device reduces to zero as the two input signals reach the same level when they are in-phase/out-phase.

In above, we assumed the devices are working at a constant temperature and did not take into account of the possible pyroelectric effect. In addition, we simplified the relations among electric field  $E$ , strain  $S$  and stress  $T$ . In general, they are coupled together in the form of  $E + \beta S + \gamma T = 0$  to the first order. Detailed analysis and expressions can be found in standard texts relating to piezoelectric materials.

The clamping itself, apart from using clamps, can be realised by using two pieces of thick material (such as substrate) on each side of the device. The inertia of such a material will act as some kind of clamp, which should be particularly effective as a fast input signal or an input pulse is concerned.

It is not necessary to clamp the driving and sensing units together directly. They can be separated from each other and connected by incompressible solid or liquid. In this case, the device can work in the same fashion as if they were clamped together directly.

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Piezoelectric ceramics can be used in the sensing unit for the comparator and the signs in front of  $V_2$  in Equations (5) and (6) will disappear in this case. Besides, piezoelectric ceramics instead of ferroelectric material can be used in any one of the two units in figure 1. The signs in Equations (1) and (2) shall change accordingly.

The common electrode described in figure 1 can be used as a common ground for both input and output signal. Alternatively, it can be used as a ground electrode only for one unit so that the corresponding signal will float on the other one. For example, the output signal can be floating on the input signal. Same argument applies to the comparator.

The clamped device described here should be affected very little by external disturbances, as long as the scale of the device concerned is much smaller than the wavelength of the acoustic wave. The internal and relative displacements during the piezoelectric operation can be analogised to the optical mode of phonons, while the external disturbance, e.g. vibrations, to the acoustic mode which should have very little impact on our output.

The foregoing description has been given by way of example only and it will be appreciated by a person skilled in the art that modifications can be made without departing from the scope of the present invention.